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shown in Fig. 5C, obtained are $0.0062pL^4/EI$ and $0.0020pL^4/EI$ as shown in Figs. 5B and 5D, respectively. In other words, as shown in Figs. 5A to 5D, it is indicated that with the same surface pressure being applied, the longer the axial length of the run-out preventing portion becomes, the smaller the pillar deforms at the ends of the run-out preventing portion. Since it was assumed in the above calculations that the roots at the pillar are free fulcrums and that the surface pressure is uniform in the axial direction, although, strictly speaking, the set environment was different from the actual case, the results of the strict calculations indicate that there is a consistent tendency that the longer the axial length of the run-out preventing portion becomes, the smaller the pillar deforms at the ends of the run-out preventing portion. When the roller is inserted into the pocket, comprehensively speaking, since the engagement margin on the pillar is deformed, to refer to the results of the above calculations in other words, with the same engagement margin, the longer the axial length of the run-out preventing portion becomes, the higher the surface pressure increases.

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Therefore, the axial length of the run-out preventing portion with which the likelihood that the roller 10 is damaged when it is inserted into the pocket is kept as low as possible while the rotating performance thereof is maintained is equal to or less than the roller effective length e and preferably 0.75 times longer than the roller effective length e . In a case where the axial length of the run-out preventing portion is set at 0.75 times or less the roller effective length e in length, when a retainer and roller assembly comprising a retainer and rollers is installed between